MULTIMEDIA		UNIVERSITY
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# **MULTIMEDIA UNIVERSITY**

# FINAL EXAMINATION

TRIMESTER 1, 2019/2020

## **BMS2024 -ADVANCED MANAGERIAL STATISTICS**

(All Sections / Groups)

19 OCTOBER 2019 2.30 pm – 4.30 pm (2 Hours)

#### INSTRUCTIONS TO STUDENTS

- 1. This question paper consists of 15 pages excluding the cover page.
- 2. This question paper consists of FOUR structured questions. Attempt ALL questions.
- 3. Students are allowed to use non-programmable scientific calculators with no restrictions.
- 4. A formulae list and statistical tables are attached at the end of the question paper.
- 5. Use pen to write the answers in the answer booklet provided.

#### **QUESTION 1 (25 Marks)**

Spam e-mail has become a serious and costly nuisance. An office manager believes that the average amount of time spent by office workers reading and deleting spam exceeds 25 minutes per day. He takes a random sample of 18 workers and measures the amount time each spends reading and deleting spam. The sample mean is 30 minutes. The population standard deviation is 12 minutes. Can the manager infer that he is correct?

- a) Establish the appropriate null and alternative hypotheses. (2 marks)
- b) Compute the test statistic and the p-value of the test. (6 marks)
- c) Based on the p-value obtained in (b), what is your statistical decision? Use  $\alpha = 0.01$ . (3 marks)
- d) State the possible Type I and Type II errors that might occur. (4 marks)
- e) At 0.05 level of significance, compute the probability of a Type II error. Given that the actual average amount of time spent reading and deleting spam is 28 minutes.

  (7 marks)
- f) Compute the power of the test. (2 marks)
- g) If the significance level is decreased, what is the effect on the power of the test.

  (1 mark)

Continued...

#### **QUESTION 2 (25 Marks)**

a) State three assumptions and one limitation for Independence t-test.

(5 marks)

b) A perfume manufacturer is trying to choose between two magazine advertising layouts. An expensive layout would include a small package of the perfume. A cheaper layout would include a 'scratch and sniff' sample of the product. The manufacturer would use the more expensive layout only if there is evidence that would lead to a higher approval rate.

The manufacturer presents the more expensive layout to four groups and determines the approval rating for each group. He presents the 'scratch and sniff' layout to five groups and again, determines the approval rating of the perfume for each group. Apply an appropriate statistical test for the listed data below at a level of significance of 0.05. Assume the listed data is non normally distributed:

Pack	age 5	2	68	43	48	] .
Scratch	37	40	53	39	4	7

(20 marks)

Continued...

#### **QUESTION 3 (25 Marks)**

Bob Stark is conducting research on monthly expenses for medical care, including over the counter medicine. His dependent variable is monthly expenses (\$) for medical care while the independent variables are number of family members, life insurance (\$) and health insurance (\$). The summary output of the analysis is shown below:

#### **ANOVA**

	df	SS	MS	F	Significance F
Regression	3	132875933	43977657	48.48745	1.21*10-7
Residual	14	126978660	906990.4		
Total	17	322909753			
	Coefficients	Std Error	t Stat	P-value	
Intercept	144.91	1025.911	0.141246		_
Family	11.63	1.247247	9.330762	2.19*10-4	
Life	13.70	8.786907	-1.55916	0.141272	
Health	-9.11	1.166068	7.810781	1.81*10 <sup>-6</sup>	

- a) State the multiple linear regression equation for the above data. (4 marks)
- b) Interpret the slope coefficient for the number of family members and health insurance relating to the monthly expenses for medical care. (4 marks)
- c) Compute the coefficient of multiple determination. Interpret the value. (4 marks)
- d) At the 5 percent level of significance, test the overall validity of the model.

  (4 marks)
- e) At the 1 percent level of significance, test if each independent variable is significantly related towards the monthly expenses for medical care. (6 marks)
- f) Determine Bob Stark's monthly expenses for his medical care if the family members are 7 persons, insured \$1377 for his life insurance and insured \$953 of his health insurance. (3 marks)

Continued...

#### **QUESTION 4 (25 Marks)**

During a study, individuals were asked to rate a product on a scale of 1-5. From the following summary output, help the researcher determine whether any significant differences exist in opinions among individuals from different regions: South, North and East. Assume that the dataset is normally distributed.

**Summary Output** 

Groups	Count	Sum	Mean	Variance
South	7	23	3.29	2.2381
North	10	29	2.90	2.3222
East	8	23	2.88	2.6964

#### **ANOVA**

Source of Variation	SS	df	MS	F
Among Groups	0.80	2	0.40	0.1653
Within Groups	53.20	22	2.42	
Total	54	24		

- a) At the 5 percent level of significance, is there evidence of a difference in the mean exist of individually opinions from the three regions regarding the product. Conduct an appropriate statistical procedure. (10 marks)
- b) Conduct the Tukey-Kramer post-hoc test to examine which region differ in mean rating the product. Use 10 percent significance level. (15 marks)

#### STATISTICAL FORMULAE

#### A. DESCRIPTIVE STATISTICS

Sample Mean = 
$$\overline{X} = \frac{\sum_{i=1}^{n} X_i}{n}$$
 Sample Standard Deviation =  $s = \sqrt{\frac{\sum_{i=1}^{n} X_i^2}{n-1} - \frac{\left(\sum_{i=1}^{n} X_i\right)^2}{n(n-1)}}$ 

where n = number of observations

 $X_i = the i^{th} observation of the data$ 

#### **B. HYPOTHESIS TESTING**

#### **Types of Error**

Type I Error =  $\alpha$ = P(Rejecting H<sub>0</sub> | H<sub>0</sub> is true) where, Confidence Interval = 1 -  $\alpha$ 

Type II Error =  $\beta$ = P(Not Rejecting H<sub>0</sub> | H<sub>0</sub> is false)

One Sample Mean Test					
σ Known	σ Unknown				
$z = \frac{\overline{x} - \mu}{\sigma / \sqrt{n}}$	$t = \frac{\overline{x} - \mu}{\sqrt[S]{\sqrt{n}}}$				

#### Two Sample Mean Test

#### Comparing Means for Two Independent Populations

#### [Standard Deviation (5) Known]

$$z = \frac{\overline{(x_1 - x_2) - (\mu_1 - \mu_2)}}{\sqrt{\sigma_1^2 / n_1 + \sigma_2^2 / n_2}}$$

#### [Standard Deviation (o) Not Known]

$$t = \frac{\overline{(x_1 - x_2)} - (\mu_1 - \mu_2)}{\sqrt{S_p^2 \binom{1}{n_1} + \frac{1}{n_2}}}$$

where 
$$S_p^2 = \frac{(n_1 - 1)S_1^2 + (n_2 - 1)S_2^2}{(n_1 + n_2 - 2)}$$

#### Two Sample Mean Test

#### **Comparing Means for Two Paired Populations**

$$t = \frac{\left(\overline{D} - \mu_D\right)}{S_D / \sqrt{n}} \qquad \text{where } \overline{D} = \frac{\sum_{i=1}^n D_i}{n} \quad \text{and } S_D = \sqrt{\frac{\sum_{i=1}^n D_i^2}{n-1} - \frac{\left(\sum_{i=1}^n D_i\right)^2}{n(n-1)}}$$

Non-Parametric Analysis							
Wilcoxon Rank Sum Test	Wilcoxon Signed Rank Sum Test						
$Z = \frac{\left(T_1 - \mu_{T_1}\right)}{\sigma_{T_1}}$ where	$Z = \frac{\left(T_{+} - \mu_{T_{+}}\right)}{\sigma_{T_{+}}} \qquad \text{where}$						
$\mu_{T1} = \frac{n_1(n+1)}{2} \qquad \text{and} \qquad$	$\mu_{T+} = \frac{n(n+1)}{4}  \text{and} $						
$\sigma_{T_1} = \sqrt{\frac{n_1 n_2 (n+1)}{12}}$ where $n = n_1 + n_2$	$\sigma_{T_{+}} = \sqrt{\frac{n(n+1)(2n+1)}{24}}$						

#### Kruskal-Wallis Rank Test

$$H = \left[ \frac{12}{n(n+1)} \sum_{j=1}^{c} \frac{T_{j}^{2}}{n_{j}} \right] - 3(n+1) \text{ where the critical value is } \chi^{2} \text{ with } df = c - 1$$

Check ranking sum:  $\sum T_j = n(n+1)/2$ 

## Chi-Square Test

$$\chi^2 = \sum_{i=1}^{n} \frac{(O-E)^2}{E}$$

where O = Frequency of Observed Values

and

E = Frequency of Expected Values

with df = c - 1

where c = number of categories

or

with df = (r-1)(c-1) where r = number of rows and <math>c = number of columns

#### C. ANALYSIS OF VARIANCE (ANOVA)

Source	Degrees of Freedom	Sum of Squares	Mean Squares	F-statistic
Among Groups	c-I	SSA	MSA = SSA/c-1	MSA/MSW
Within Groups	n - c	SSW	MSW = SSW/n-c	
Total	n - 1	SST		

$$SST = \sum_{j=1}^{c} \sum_{i=1}^{n_{j}} \left( X_{ij} - \overline{X} \right) \text{ or alternative formula:}$$

$$SST = \left( \sum_{j=1}^{c} \sum_{i=1}^{n_{i}} X_{ij}^{2} \right) - \frac{\left( \sum_{j=1}^{c} \sum_{i=1}^{n_{i}} X_{ij}^{2} \right)}{n}$$

$$SSA = \sum_{i=1}^{c} n_{j} \left( \overline{X}_{j} - \overline{X} \right)^{2} \text{ and } SSW = SST - SSA$$

where n = number of observations, c = number of groups and  $\overline{X} = overall$  mean

#### Tukey-Kramer Procedure

Critical Range = 
$$Q_U \sqrt{\frac{MSW}{2} \left[ \frac{1}{n_i} + \frac{1}{n_j} \right]}$$

where  $Q_u =$  the upper tail critical value from a Studentized Range Distribution having (c) degrees of freedom in the numerator and (n-c) degrees of freedom in the denominator at a given level of significance

Two-Way	ANOVA	y fariyaya sa		
Source	Degrees of Freedom	Sum of Squares	Mean Squares	F-statistic
Α	r-1	SSA	MSA = SSA/(r-1)	MSA / MSE
В	c -1	SSB	MSB = SSB/(c-I)	MSB / MSE
AB	(r-1)(c-1)	SSAB	MSAB = SSAB/(r-1)(c-1)	MSAB / MSE
Error	rc (n -1)	SSE	MSE = SSE/rc(n'-1)	
Total	n-1	SST		<u> </u>

where,

Factor A levels are represented by the rows and Factor B levels are represented by the columns and

n = number of observations

c = number of columns

r = number of rows

n' = number of replicates

$$SST = \sum_{i=1}^{r} \sum_{i=1}^{c} \sum_{k=1}^{n'} \left( X_{ijk} - \overline{\overline{X}} \right)^{2} \qquad SSA = cn' \sum_{i=1}^{r} \left( \overline{X}_{i} - \overline{\overline{X}} \right)^{2}$$

$$SSB = rn \sum_{j=1}^{c} \left( \overline{X} j - \overline{\overline{X}} \right)^{2} \qquad \text{where } \overline{\overline{X}} = overall \ mean$$

 $SSE = (n'-1)[S_1^2 + S_2^2 + \dots + S_k^2]$  where  $S_i^2$  = variance of each block

#### D. REGRESSION ANALYSIS

#### Multiple Linear Regression

Population Model:  $Y = \beta_0 + \beta_1 X_1 + \beta_2 X_2 + \dots + \beta_k X_k + \varepsilon$ 

Sample Model:  $y = b_0 + b_1 x_1 + b_2 x_2 + \dots + b_k x_k + e$ 

Adjusted R-Square =  $1 - \left[ \frac{(1-R^2)(n-1)}{(n-p-1)} \right]$  where p = number of independent/predictor variables

ANOVA Table for Regression							
Source	Degrees of Freedom	Sum of Squares	Mean Squares				
Regression	p	SSR	MSR = SSR/p				
Error/Residual	n-p-1	SSE	MSE = SSE/(n-p-1)				
Total	n-1	SST					

Test Statistic for Significance of the Overall Regression Model F = MSR/MSE

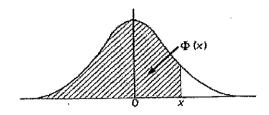
## Test Statistic for Significance of Each Predictor Variable

$$t_i = \frac{b_i}{S_{b_i}}$$
 and the critical value =  $\pm t_{\alpha/2,(n-p-1)}$ 

# TABLE 4. THE NORMAL DISTRIBUTION FUNCTION

The function tabulated is  $\Phi(x) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{x} e^{-\frac{1}{2}t^2} dt$ .  $\Phi(x)$  is

the probability that a random variable, normally distributed with zero mean and unit variance, will be less than or equal to x. When x < 0 use  $\Phi(x) = 1 - \Phi(-x)$ , as the normal distribution with zero mean and unit variance is symmetric about zero.



æ	$\Phi(x)$	x	$\Phi(x)$	æ	$\Phi(x)$	x	$\Phi(x)$	æ	$\Phi(x)$	x	$\Phi(x)$
0.00	0.2000	0.40	0.6554	0.80	0.7881	I.50	0.8849	x-60	0.9452	2.00	0.97725
.01	15040	·41	6591	·81	7010	:2X	-8869	-6x	9463	OI	.97778
-02	-5080	.42	·6628	·8 <b>2</b>	7939	.32	-8888	-62	9474	'02	·97831
.03	-5120	43	·6664	.83	7967	· <b>2</b> 3	-8907	63	19484	.03	·9788 <b>2</b>
-04	-5160	44	6700	·8 <b>4</b>	.7995	.24	-8925	-64	·9495	*04	97932
0.02	0-5199	0.45	0.6736	0.85	0.8023	1.25	0.8944	1.65	0.9502	2.02	0.97982
-06	5239	46	6772	.86	-805¥	-26	·8962	-66	9515	-06	.98030
-07	.5279	47	6808	·8 <sub>7</sub>	-8078	.27	-8980	-67	19525	.07	.98077
-08	.2318	-48	•6844	-88	8106	·28	-8997	-68	'9535	80.	98124
-09	5359	-49	6879	.89	·8133	.59	-9015	-69	'9545	·09	-98169
0.10	0.5398	0.20	0.6912	0.90	0.8159	1.30	0.9032	1.70	0.9554	2.10	0.98214
·xx	.5438	·51	·695a	.6x	.8186	-31	.9049	<b>-7</b> x	9564	.II.	-98257
12	·5 <del>4</del> 78	.52	-6985	.02	.8212	*32	~90 <u>6</u> 6	.72	'9573	.12	-98300
.13	'5517	.53	.7019	.93	8238	*33	-9082	.73	9582	.13	-98341
.14	5557	.54	7054	<b>'94</b>	8264	<b>*34</b>	-9099	'74	.9591	-14	-98382
o-x5	0:5596	0.55	0.7088	0.02	0.8289	1.35	0.0112	1.75	0.9599	2.12	0.98422
.16	-5636	-56	7123	-96	8315	•36	.0131	·76	9608	·16	19846x
·x7	.5675	57	7157	-97	8340	<b>.</b> 37	.9147	`77	19616	.17	-98500
8r.	5714	-58	7190	-98	-8365	-38	-9162	.78	9625	.r8	-98537
.19	5753	59	7224	*99	-8389	-39	9177	'79	9633	-r9	·98574
0.20	9.5793	0.60	0.7257	1.00	0.8413	1.40	0.9192	r·80	0.9641	2:20	0.98610
·21	15832	-6x	*729x	·OI	8438	·41	-9207	-8x	9649	·2I	.08645
.33	·5871	-62	*7324	.03	8461	·42	9222	-82	9656	-22	-98679
<b>-23</b>	-5910	∙6ვ	7357	-03	8485	43	-9236	83	9664	'23	98713
'24	·5948	·6 <sub>4</sub>	-7389	<b>'04</b>	-8508	* <del>44</del>	·9251	-84	·9671	·24	*98745
0.25	0.5987	0.65	0.7422	1.05	0.8531	1:45	0.9265	r·85	0.9678	2.25	0-98778
-26		-66	*7454	-06	8554	· <b>4</b> 6	9279	∙86	•9686	.26	-98809
-27	6064	-67	-7486	-07	8577	*47	-9292	·8 <del>7</del>	-9693	*27	98840
·28	6103	∙68	-7517	-08	8599	·48	-9306	∙88	-9699	.28	-98870
-29	·6141	·69	*7549	-09	8621	· <del>149</del>	-9319	-89	-9706	-29	·98899
0.30	0.6179	0.70	o-7580	1.10	0.8643	1.20	0-9332	x-90	0.9713	2:30	0.98928
.3x	6217	·7x	-7611	·II	8665	-51	<sup>-</sup> 9345	-9 <b>1</b>	9719	-3I	98956
.32	-6255	.72	•7642	12	-8686	-52	*9357	-92	9726	-3≉	.08083
.33	-6293	.73	•7673	.13	8708	·53	-9370	793	9732	<sup>-</sup> 33	.030010
34	·6331	·7 <del>4</del>	17704	.14	8729	.54	-9382	194	-9738	*34	-99036
0.35	o•6368	0.75	0.7734	1.12	0.8749	1.22		1-95	0.9744	2.35	0.00061
-36	6406	.76	·7764	-16	·8770	-56	-94 <del>0</del> 6	-96	-9750	-36	199086
37	6443	.77	<b>.</b> 7794	.17	-8790	·57	-9418	-97	9756	37	.00111
-38	6480	.78	.7823	.18	48810	-58		-98	9761	-38	99134
.39	6517	.79	~7852	.19	-8830	·59	·944I	799	9767	-39	.99158
0.40	0.6554	0.80	0,4881	I-20	0.8849	z-60	0.9452	2.00	0-9772	2:40	0-99180

NMI

### TABLE 4. THE NORMAL DISTRIBUTION FUNCTION

æ	$\Phi(x)$	æ.	$\Phi(x)$	æ	$\Phi(x)$	æ	$\Phi(x)$	æ	$\Phi(x)$	æ	$\Phi(x)$
2.40	0.00180	<b>2</b> ·55	0.99461	2.70	o-99653	2.85	o-99781	3.00	o-9986 <u>s</u>	3.12	o-99918
<b>'4</b> I	-99202	-56	99477	·71	199664	∙86	-99788	101	99869	·16	99921
•42	.09224	.57	199492	.72	·99674	·8 <sub>7</sub>	199795	-02	99874	·17	99924
*43	·99245	·58	199506	.73	199683	∙88	·99801	.03	99878	-18	99926
·44	·99 <del>2</del> 66	<b>·</b> 59	199520	·7 <del>4</del>	-99693	.89	-99807	.04	99882	.10	99929
2.45	0.99286	2-60	0.99534	2.75	0100702	2.00	0.99813	3.02	0199886	3.20	0*99931
-46	-99305	·6x	.99547	.76	99711	.01	.00810	-06	99889	-21	99934
47	199324	.62	199560	-77	99720	-92	.99825	.07	.99893	*22	99936
-48	199343	¹63	199573	٠78	.99728	•93	12899	-08	99896	-23	99938
· <b>49</b>	·99361	-64	199585	.79	199736	.94	99836	.09	.99900	24	99940
2.50	0.99379	2.65	0.99598	2.80	O199744	2.95	0.00841	3.10	0.99903	3 25	0.99942
-51	-99396	-66	•99609	·81	99752	-96	99846	11	-99906	26	99944
·52	199413	∙67	·99621	·82	99760	.97	199851	12	99910	.27	99946
53	199430	.68	99632	.83	99767	-98	·99856	13	99913	28	799948
<sup>-</sup> 54	·99446	· <del>6</del> 9	99643	-84	99774	-99	·99861	14	99916	29	99950
2.55	0-9946x	2.70	0-99653	2.85	0-99781	3.00	o-9986 <u>5</u>	3-15	0.99918	3.30	0.99952

The critical table below gives on the left the range of values of x for which  $\Phi(x)$  takes the value on the right, correct to the last figure given; in critical cases, take the upper of the two values of  $\Phi(x)$  indicated.

2:075	3·263 0·9995 3·320 0·9995	3.731 0.99990 3.759 0.99992 3.791 0.99993 3.826 0.99993	3.916 0.99995
2 2 4 2 0.9990	3 203 0.9995	3 /32 0.09991	3 910 0 99996
3 203 0-9991	3.320 0-9996	3 /39 0.99992	3'970 0'99997
3"130 0.9992	3.389 0.9996 3.480 0.9997	3.791	4-055 0-00008
3'174 0'0003	3.480 0.0008	3.826 0.00004	4°×73 0'00000
3.075 3.105 3.138 0.9992 3.174 0.9993 3.215 0.9994	3.6x2 0.0008	3.867 0.99994	3 976 0 99996 3 976 0 999997 4 055 0 999998 4 173 0 999999 4 417 1 00000

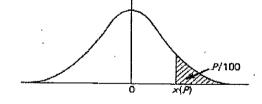
When x > 3.3 the formula  $1 - \Phi(x) = \frac{e^{-1x^2}}{x\sqrt{2\pi}} \left[ 1 - \frac{1}{x^2} + \frac{3}{x^4} - \frac{15}{x^6} + \frac{105}{x^8} \right]$  is very accurate, with relative error less than  $945/x^{10}$ .

# TABLE 5. PERCENTAGE POINTS OF THE NORMAL DISTRIBUTION

This table gives percentage points x(P) defined by the equation

$$\frac{P}{100} = \frac{1}{\sqrt{2\pi}} \int_{-\pi(P)}^{\infty} e^{-\frac{t}{2}t^2} dt.$$

If X is a variable, normally distributed with zero mean and unit variance, P/100 is the probability that  $X \ge x(P)$ . The lower P per cent points are given by symmetry as -x(P), and the probability that  $|X| \ge x(P)$  is 2P/100.



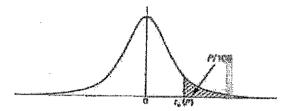
P	x(P)	P	x(P)	$\boldsymbol{P}$	x(P)	$\boldsymbol{P}$	x(P)	$\boldsymbol{P}$	x(P)	$\boldsymbol{P}$	x(P)
50	0.0000	5.0	1-6449	3.0	1 8808	2.0	2.0537	1.0	2.3263	0.10	3.0002
45	0.1257	4.8	1.6646	2.9	1.8957	1.9	2:0749	0.0	2-3656	9.09	3.1214
40	0.2533	4.6	1-6849	2.8	1.9110	x-8	<b>2.</b> 0969	6.8	2.4089	9∘0	3'1559
35	0.3823	4.4	1-7060	2.7	1-9268	1.7	2.1201	0.7	<del>2</del> *4573	0.07	3.1947
30	0.244	4.3	1.7279	2.6	1,0431	<b>1.</b> 6	21444	0.0	2-5121	0.06	3.5380
25	0.6745	4.0	117507	2.2	119600	1.2	2.1701	0.2	2-5758	0.02	312905
20	0.8416	3.8	1*7744	24	I 9774	1.4	2.1973	0.4	2.6521	0.01	3.4100
15	1.0364	3.6	1.7991	2.3	T 9954	1.3	2.2262	0.3	2.7478	0.002	3.8906
10	1.5816	3.4	1.8220	2.2	2.0141	1.2	2.2571	0.2	2.8782	0.00r	4.2640
5	1.6449	3.2	1.8522	3.I	2.0332	1.1	2.2904	D.I	3.0902	0.0002	414172

## TABLE 10. PERCENTAGE POINTS OF THE t-DISTRIBUTION

This table gives percentage points  $t_r(P)$  defined by the equation

$$\frac{P}{100} = \frac{1}{\sqrt{\nu\pi}} \frac{\Gamma(\frac{1}{2}\nu + \frac{1}{2})}{\Gamma(\frac{1}{2}\nu)} \int_{t_p(P)}^{\infty} \frac{dt}{(\mathbf{1} + t^2/\nu)^{\frac{1}{2}(\nu+1)}},$$

Let  $X_1$  and  $X_k$  be independent random variables having a normal distribution with zero mean and unit variance and a  $\chi^a$ -distribution with  $\nu$  degrees of freedom respectively; then  $t = X_1/\sqrt{X_2/\nu}$  has Student's t-distribution with  $\nu$  degrees of freedom, and the probability that  $t \ge t_{\nu}(P)$  is P/100. The lower percentage points are given by symmetry as  $-t_{\nu}(P)$ , and the probability that  $|t| \ge t_{\nu}(P)$  is 2P/100.



The limiting distribution of t as  $\nu$  tends to invinity is the normal distribution with zero mean and unit varience. When  $\nu$  is large interpolation in  $\nu$  should be harmonic.

P	40	30	25	20	15	TO	5	2.2	x	0.2	0.1	0.02
$v = \tau$	0.3249	0.7265	1.0000	1.3764	1.063	3.078	6-314	12.71	31.82	63.66	318-3	.636.6
2	0.2887	0.6172	0.8165	1.0607	1.386	1-886	2-920	4.303	6.065	9.925	22:33	31.60
. 3	0.2767	0.5844	0 7649	0.9785	1.250	1.638	2.353	3.185	4.241	5.841	10.31	12.02
· 4	0-2707	0.2686	0.7407	0.0410	1.100	1.233	2-132	2.776	3.747	4.604	7'173	8.610
								•••			• 7.7	4 7 2 3
5 6	0.5623	0.5594	0.7267	0.9195	1.126	1.476	2.015	2'571	3.362	4.032	5.893	6.869
6	o <sup>.</sup> 2648	O·5534	0.7176	0.9057	1.134	1.440	1.943	2.447	3.143	3.707	5-203	5.959
7	0.5635	0.249x	0.7111	0.8960	1.110	1.412	j·895	2.362	· 2·998	3'499	4.78.	5.408
8	0.5610	0.5459	0.7064	o-8889	1.108	I:397	1-86o	2:306	2:896	3.352	4'50.	5.041
9	0.5610	0.5435	0.7027	0.8834	1.100	1.383	1.833	2,565	2·82 <sub>.</sub> 1	3.520	4'29''	4·781
10	0.2602	0.5415	0.6998	0-8791	1003	r-372	1.812	2.228	2.764			
II	0.2596	0.2300	0.6974	0.8755	1.088	1.363	1.796	2.301	2.718	3.160	4.144	4.587
12	0.520	05386	0.6955	0.8726	1-083	1.356	1782	2.120	2.681	3-106	4.02	4.437
<b>I</b> 3	0.2586	0.5375	0.6938	0.8702	1 079	1.320	1.771	2.160	2.620	3.022	3.930	4'318
14	0.5285	0.5366	0.6924	0.8681	1.076	1-345	1.761	2 145	2.624	_	3.85:: 3.78:	4.221
-4	4 <b>-</b> 30÷	0 3300	OOgaq	0 0001	1 0,0	* 373	4 /01	2 143	2 024	2.977	3.70	4.140
IS	0.2570	0.2322	0.6912	0.8662	1.074	1'34I	1.753	2.131	21602	2.947	3.733	4.073
<b>16</b>	0.2576	0.2320	о боот	0.8647	1.071	x:337	1.746	2.120	2.583	2.021	3.686	4'015
17	0.2573	0.5344	0.6892	0.8633	1.069	1.333	1.740	2'110	2.567	2.808	3.646	3.965
18	0.2571	0.5338	0.6884	0.8620	1 067	1.330	1.734	2.101	2'552	2.878	3.61c	3.922
19	0.2569	O:5333	0.6876	0.8610	1 066	1.328	1:729	2.093	2.239	2.861	3.579	3.883
	_								_	_		
20	0.2567	0.2356	0.6870	0-8600	1.064	1.322	7.725	2.086	2.228	2.845	3.225	3.850
21	0.2566	0.2322	0.6864	0 8591	1.063	1.353	1.721	2.080	2.218	2.831	3.222	3.810
22	0.2564	0.2321	0.6828	0-8583	1.001	1.321	1.212	2.074	2.208	2.819	3.202	3.792
23	0.2563	0.2314	0.6823	0.8575	1.000	1.310	1714	2.069	2.500	2.807	3.485	3.768
24	0.2562	0.2314	0.6848	0.8569	1.059	1.318	1,411	2.064	2.492	2.797	3.467	3.745
25	0.2561	0.5312	0.6844	0.8562	r.058	1.316	11708	2.060	2.485	2.787	3.450	3.725
26	0.2560	0.5309	0.6840	0.8557	1.028	1.312	1.706	2.056	2'479	2.779	3.435	3.202
27	0.2559	0.2306	0.6837	0.8551	1.057	1.314	1 703	2.052	2.473	2.771	3.421	3.69c
28	0.2528	0.2304	0.6834	0.8546	1 056	1.313	1.701	2.048	2.467	2:763	3.408	3.674
29	0.2557	0.2302	0.6830	0.8542	1.055	1.311	x 699	2.045	2.462	2.756	3.396	3.620
		- 00			•						-	
30	0.2556	0.2300	o·6828	0.8538	1.055	1.310	1 697	2.042	2.457	2.750	3.382	3.646
32	0.2555	0.5297	0.6822	0.8530	1.054	1.300	1.694	2.037	2.449	2.738	3.365	3.622
34	0.2553	0.2294	0.6818	0.8523	1.025	1.302	1,601	2.032	2°44I	2.728	3 348	3.601
36	0.2552	0.2291	0.6814	0.8517	1 052	1-306	1-688	2.028	2.434	2.710	3.333	3.285
38	0.5221	0.5288	0.6810	0.8512	1.021	1.304	<b>z⊦686</b>	2 024	2.429	2.413	3.310	3.266
			ر م				zl 684			0.55	A.c	4
40	0.2550	0.5286	0.6807	0.8202	1.050	1.303		2.021	2'423	2.704	3 307	3.221
50	0.2547	0.5278	0.6794	0.8489	1 047	1,500	1 676	2.000	2.403	2:678	3,561	3:496
60	0-2545	0'5272	0.6786	0.8477	1.045	1.506	1-671	2.000	2:390	2.660	3.232	
120	0.523	0.2228	o 6765	0.8446	I.O4I	1-289	ı⊦6 <u>5</u> 8	1.080	2.328	2.617	3.120	3.373
80	0.2533	0.5244	0.6745	0.8416	1.036	1.282	ı <b>⊦64</b> 5	1.960	2-326	2.576	3.090	3.591

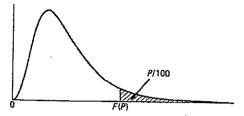
# TABLE 12(a). 10 PER CENT POINTS OF THE F-DISTRIBUTION

The function tabulated is  $F(P) = F(P|\nu_1, \nu_2)$  defined by the equation

$$\frac{P}{100} = \frac{\Gamma(\frac{1}{2}\nu_1 + \frac{1}{2}\nu_2)}{\Gamma(\frac{1}{2}\nu_1) \Gamma(\frac{1}{2}\nu_2)} \nu_1^{\frac{1}{2}\nu_1} \nu_2^{\frac{1}{2}\nu_2} \int_{F(P)}^{\infty} \frac{F^{\frac{1}{2}\nu_1 - 1}}{(\nu_2 + \nu_1 F)^{\frac{1}{2}(\nu_1 + \nu_2)}} dF,$$

for P=10, 5, 2.5, 1, 0.5 and 0.1. The lower percentage points, that is the values  $F'(P)=F'(P|\nu_1,\nu_2)$  such that the probability that  $F\leqslant F'(P)$  is equal to P/100, may be found by the formula

$$F'(P|\nu_1, \nu_2) = 1/F(P|\nu_2, \nu_1).$$

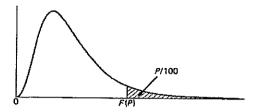


(This shape applies only when  $\nu_1\geqslant 3$ . When  $\nu_1<3$  the mode is at the origin.)

$\nu_1 =$	r	2	3	4	5	6	7	8	10	12	24	80
$v_2 = 1$	~ -	49.50	53:59	55.83	57:24	58.20	58.91	59.44	60.10	60.41		
2	8.526	9.000	9.162	9.243	9.293	9.326	9:349	9'367	9.392		62.00	63.33
3	5.238	5.462	2.391	5.343	5.309	5.285	5.566	5'252	5.230	9.408 5.216	9.450	9.491
4	4.242	4.322	4.101	4.102	4'051	4.010	3.235	3.955	3-920	3.896	5.176	5.134
					• •	-y	2 313	3 933	3 920	3.090	3.831	3.761
5	4.060	3.780	3.619	3.20	3'453	3.405	3.368	3:339	3*297	3.268	3,101	
6	3.776	3.463	3.580	3.181	3.108	3.055	3'014	2.083	2.032	2.002	2.818	3.102
7	3.286	3*257	3'074	2.961	2.883	2.827	2.785	2.752	2·703	2.668		2.722
8	3 458	3.113	2.924	2-806	2.726	2.668	2.624	2.589	2.238	2.202	2.575	2.471
. 9	3.300	3 000	5.813	2-693	2,611	2-551	2.202	2.460	2.416	2.379	2 404 2 277	2.293
	_						- 5-5	~ 7-7	~ 724	w 379	4 +77	2.123
10	3-285	2.924	2.728	2.602	2.222	2.461	2.414	2:377	2.323	2-284	2.178	2.055
II	3-225	2.860	2.660	2.236	2.451	2.389	2.342	2.304	2:248	2.200	2,100	1.972
12	3.177	2.807	2.606	2.480	2.394	2.331	2.283	2.245	2.188	2.147	2.036	1.004
13	3,136	2.763	2,260	2.434	2.347	2.283	2'234	2.192	2.138	2.097	1.083	1.846
14	3.105	2.726	2.252	2.395	2:307	2'243	2-193	2.124	2.002	2.054	1.938	1.797
										54	- 930	* 191
15	3.073	2.695	2.490	2.361	2.273	2.208	2.128	2.110	2.050	2'017	1.800	1.755
16	3 048	2-668	2'462	2,333	2'244	2.178	2.128	2.088	2.028	1.085	1.866	1.718
17	3.026	2.645	2.437	2,308	5.518	2.125	2.102	2.061	2.001	1.958	1.836	1.686
18	3 00 7	2.624	2.416	2.286	2.196	2,130	2.079	2.038	1.977	1.033	1.810	1.657
19	2.990	2-606	2.397	2.266	2.176	2.100	2.058	2'017	1.926	1.012	1.787	1.631
		0	^					-	• •	•	, - ,	·· - J-
20	2.975	2.289	2.380	2'249	2.128	2.001	2.040	1.999	1.937	1.892	1.767	1.607
21 22	2.961	2.275	2.365	2.533	2.142	2.075	2.023	1.982	1.920	1.875	1-748	1.286
23	21949	2.561	2.32I	2.219	2.158	2.000	21008	1.967	1.004	1.859	1.731	1.262
24	2.037	2.249	2.339	2.207	2.112	2.04.2	1.995	1.953	1.890	1.845	1.716	1.249
~4	2.927	2.238	21327	5.192	2.103	2.032	1.983	1.041	1.877	1.832	1.702	1.233
25 .	2.018	2.528		0 -							•	***
26	2.000	2.210	2.317	2.184	2.002	2.024	1.971	1.929	1.866	1.820	1.689	1.218
27	5.001	2.211	2.302	2.174	2.082	2.014	1.961	1.919	1.855	1.809	1.677	1.204
28	2.894	2.203	2:299	2.162	2.073	2.002	1.952	1.000	1.845	1.799	1.666	1.491
20	2.887	2.495	2·291 2·283	2.157	2.064	1.000	1.043	1,000	1-836	1.790	1.656	1'478
-3	- 40,	4475	2 205	2.140	2.057	1.988	1.932	1.892	1-827	1.781	1.647	1'467
30	2·881	2-489	2.276	2-142		0			_			
32	2.860	2.477	2.263	•	2.040	1.980	1.927	1.884	1.810	1.773	1.638	1,426
34	2.859	2.466	2.252	2·118	2.036	1.967	1.913	1.870	1.805	1.758	1.622	1.437
36	2.850	2,456	2.243	2.108	2.024	1.955	1.001	1.858	1.793	1.745	1.608	1 419
38	2.842	2'448	2.234	2.000	2.014	1.945	1.801	1.847	1.481	1.734	1.595	1'404
•	• •	- 44-	~ -3+	- 099	2.005	1.935	1.881	1.838	1.772	1.724	1-584	1,300
40	2.835	2.440	2.226	2.001	1.997	Tinon		- 0				
60	2.201	2:393	2.177	2.041	1.946	1·927 1·875	1.873	1-829	1-763	1.715	I.274	1.377
120	2.748	2°347	2,130	1.992	1.896	1.824	1.819	1.775	1"707	1.657	1.211	1.501
ø	2.706	2.303	2.084	1 992 1 945	1-847	•	1-767	1.722	1-652	1.601	1'447	1.103
	-			- 543	* 041	1.774	1-717	1-670	1-599	1.546	1.383	1.000

## TABLE 12(b). 5 PER CENT POINTS OF THE F-DISTRIBUTION

If  $F = \frac{X_1}{\nu_1} / \frac{X_2}{\nu_2}$ , where  $X_1$  and  $X_2$  are independent random variables distributed as  $\chi^2$  with  $\nu_1$  and  $\nu_2$  degrees of freedom respectively, then the probabilities that  $F \geqslant F(P)$  and that  $F \leqslant F'(P)$  are both equal to P/100. Linear interpolation in  $\nu_1$  and  $\nu_2$  will generally be sufficiently accurate except when either  $\nu_1 > 12$  or  $\nu_2 > 40$ , when harmonic interpolation should be used.



(This shape applies only when  $v_1 \geqslant 3$ . When  $v_1 < 3$  the mode is at the origin.)

$\nu_1 =$	I	2	3	4	5	6	7	8	IO	12	24	80
$v_2 = r$	161-4	199.5	215.7	224.6	230.2	234.0	236-8	238.9	241'9	243.0	249.1	25413
2	18.21	19-00	19-16	19.25	19.30	19.33	19:35	19:37	19.40	10.41	19.45	19.50
3	10-13	9.552	9-277	9.117	0.013	8.941	8.887	8.845	8.786	8.745	8.630	8:526
4	7.709	6.944	6·591	6.388	6-256	6.163	6.094	6.041	5.964	5'912	5.774	5.628
			•					•			~	
5	6.608	5.786	5.409	5.192	5,020	4.020	4.876	4.818	4.735	4.678	4.227	4.365
6	5.987	5.143	4'757	4.534	4.387	4.284	4.502	4.147	4 060	4.000	3.841	3-669
7	2.201	4.737	4.342	4.150	3.972	3.866	3.787	3.726	3.637	3.575	3.410	3.530
8	2.318	4 459	4.066	3-838	3.687	3.281	3.200	3.438	3.347	3.284	3-115	2.928
9	5-117	4.256	3.863	3,633	3.482	3.374	3.593	3.530	3.137	3.023	2.900	2.707
			0		_							
IG	4.965	4 103	3.708	3.478	3.326	3.512	3.132	3.072	2.978	2.913	2.737	2.538
11	4.844	3.982	3.282	3.357	3.504	3.095	3.015	2.948	2.854	2.788	2.609	2.404
12	4.747	3 885	3.490	3.529	3.100	2.996	2.913	2 849	2 753	2.087	2.502	2.296
13	4.667	3.806	3.411	3.179	3.022	2.915	2.83 <del>2</del>	2.767	2.671	2-604	2.420	2-206
14	4.000	3.739	3°3 <del>44</del>	3.115	2.958	z·848	2.764	2.699	2.602	2.234	2.349	5.131
T	*****	3.682	2.282									
15 16	4.243	<del>-</del> .	3.287	3.056	2.901	2.790	2.707	2.641	2.244	2.475	2-288	2.066
17	4.494	3.634	3*239	3.007	2·852 2·810	2.741	2.657	2.201	2.494	2.425	2.532	2.010
18	4.451	3.202	3.197	2.965		2.699	2.614	2.548	2.420	2.381	2.100	1.960
	4·414 4·381	3.555	3.120	2.928	2.773	2.661	2.577	2.210	2.412	2.342	2.120	1.917
19	4 301	3.22	3127	2.895	2.740	2.628	2.544	2.477	2.378	2-308	2.114	1.878
20	4.321	31493	3-098	2.866	2-711	2,299	2.214	2:447	2.348	2-278	2.082	1.843
21	4'325	3.467	3.072	2.840	2.685	2.23	z·488	2'420	2.321	•		1 812
22	4.301	3 443	3*040	2.817	2.661	2.249	2.464	2.397	2.207	2·250 2·226	2·054 2·028	1.783
23	4.279	3.422	3.028	2.796	2.640	2.28	2.442	2.375	2.275	2'204	2.002	
24	4.260	3.403	3.000	2.776	2.621	2.508	2.423	2.355	2.255	2.183	1.084	1.757
		<b>5</b> 7−0	J	- //-		- 3		~ 333	2 233	2 103	1 904	1.733
25	4.242	3.382	2-991	2.759	2.603	2.490	2:405	2:337	2.236	2.165	1.964	1.711
26	4.225	3,369	2.975	2.743	2.587	2.474	2.388	2.321	2.220	2.148	1'946	1.691
27	4.510	3.354	· 2·960	2.728	2.22	2.459	2:373	2.302	2.204	2.132	1.930	1.672
28	4.196	3.340	2.947	2.714	2.558	2.445	2.359	2.291	2-190	2.118	1'915	1.654
29	4-183	3.328	2.934	2.701	2.242	2-432	2.346	2.278	2.177	2-104	1.001	1.638
									•	•		- 5-
30 -	4-171	3.316	21922	2.690	2*534	2.421	2'334	2.266	2.162	2.002	1.887	1.622
32	4.140	3.502	2.001	2.668	2*512	2.399	2.313	2.244	2'142	2.070	1.864	1.594
34	4.130	3.276	2.883	2-650	2*494	2.380	2.294	2.222	2.153	2.020	1.843	1.569
36	4.113	3.529	2.866	2.634	2-477	2.364	2.277	2.209	2.106	2.033	1.824	1 547
38	4.098	3.242	2.852	2.619	2.463	2-349	2.262	5.104	2.001	2.017	1.808	1.227
	0-		- 0	- 6.6			•					
40	4.085	3.535	2.839	2,606	2.449	2.336	2.249	2.180	2.077	2.003	1.793	1.500
60	4-001	3.120	2.758	2.525	2.368	2.254	2.102	2.097	1.993	1.917	1.700	1.380
120	3.020	3.072	2.680	2.447	2.290	2.175	2.087	2 016	1,010	1.834	1-608	1.254
90	3-841	2.996	2.602	2.372	2.514	2.099	2.010	1.038	1.831	1.752	1.217	1,000

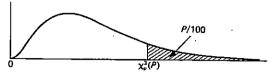
#### TABLE 8. PERCENTAGE POINTS OF THE x²-DISTRIBUTION

This table gives percentage points  $\chi^2_{\nu}(P)$  defined by the equation

$$\frac{P}{100} = \frac{1}{2^{\nu/2} \; \Gamma(\frac{\nu}{2})} \int_{\chi^2_{\nu}(P)}^{\infty} x^{\frac{1}{4}\nu - 1} \, e^{-\frac{1}{4}x} \, dx.$$

If X is a variable distributed as  $\chi^2$  with  $\nu$  degrees of freedom, P/100 is the probability that  $X \geqslant \chi^2_{\nu}(P)$ . For  $\nu > 100$ ,  $\sqrt{2X}$  is approximately normally distributed

with mean  $\sqrt{2\nu-1}$  and unit variance.



(The above shape applies for  $\nu \gg 3$  only. When  $\nu < 3$  the mode is at the origin.)

_						•					
$\boldsymbol{P}$	50	40	30	20	10	5	2.2	I	0.2	0.1	0.02
$\nu = r$	0.4549	0.7083	1.074	1.642	2.706	3·841	5.024	6.635	7.879	10.83	12.12
2	r-386	1-833	2.408		4 605	2.991	7.378			13.82	15.20
3	2.366	2.946	3.665	4.642	6.251	7·815	9.348	11.34	12.84	16.27	17.73
4	3:357	4.042	4.878	5.080	7.779	9.488	11.14	13.28	14.86	18.47	20.00
							•	•	-	• • • • • • • • • • • • • • • • • • • •	
5 6	4.321	5.133	6.064	7-289	9-236	11.07	12.83	15.09	16.75	20.52	22.11
	5.348	6.211	7.231	8.558	10.64	12.59	14.45	16.81	18.55	22:46	24.10
7	6.346	7.283	8.383	9.803	12.02	14.07	16.01	18-48	20.28	24.32	26.02
8	7:344	8·351	9.524	11.03	13.36	15.21	17:53	20.09	21.95	26.12	27.87
9	8.343	9-414	10.66	12.24	14.68	16.92	19.02	21.67	23.20	27.88	29.67
10	9:342	10.47	11.78	13.44	15.99	18-31	20.48	23.21	05:10	20.50	07.40
II	10.34	11.23	12.90	14.63	17.28	19.68	21.92	24.72	25·19 26·76	31·26 29·59	31.42
12	11.34	12.28	14.01	15.81	18-55	21.03	23.34	26.22	28-30	32.91	33·14 34·82
13	12:34	13.64	15.12	16.98	19.81	22.36	~3 34 24:74	27.69	20 30	34.23	36.48
14	13.34	14.69	16.22	18.12	21.06	23.68	26.15	27 09	31.35	36·12	38·11
	-5 54	-4 43		1013	41 00	23 00	2012	49 14	31 32	30 12	30-11
15	14.34	15.73	17:32	19.31	22.31	25.00	27:49	30.28	32.80	37.70	39.72
16	15.34	16.78	18.42	20.47	23.54	26.30	28.85	32.00	34.27	39.5	41.31
17	16.34	17.82	19.21	21.61	24.77	27.59	30.10	33.41	35.72	40.79	42.88
18	17.34	18-87	20-60	22.76	25.99	28.87	31.23	34.81	37.16	42.31	44'43
19	18.34	10.01	21.69	23.90	27:20	30.14	32.85	36.19	38-58	43.82	45 97
											• 1
20	19.34	20.95	22.77	25.04	28.41	31-41	34.12	37.57	40.00	45°31	47.50
21	20.34	21.99	23-86	26.17	29.62	32.67	35.48	38.93	41.40	46·8o	49.01
. 22	21.34	23.03	24.94	27.30	30-81	33.92	36.78	40.29	42.80	48.27	50.21
23	22.34	24.07	26-02	28.43	32.01	35'17	38∙08	41.64	44-18	49.73	52.00
24	23.34	25.11	27.10	29.55	33.50	36.42	39.36	42.98	45.26	51.18	53.48
25	24.34	26.14	28.17	30.68	34.38	37.65	40 65	44.31	46.93	52.62	54.95
26	25.34	27.18	29-25	31.79	35.26	38.89	41.92	45 64	48.29	54.02	56·41
27	26.34	28.21	30-32	32.01	36.74	40.11	43.10	46.96	49.64	55.48	57.86
28	27:34	29.25	31.30	34.03	37.92	41.34	44.46	48.28	50:99	56.89	20.30
29	28.34	30.28	32.46	35.14	39.09	42.26	45.72	49.59	52.34	58.30	60.73
•		-	• •		-, ,	• • •	15 /-	, T2 J2	J- J+	3- 3-	73
30	29.34	31.32	33-53	36-25	40.26	43.77	46.98	50.89	53.67	59.70	62-16
3 <del>2</del>	31.34	33:38	35.66	38.47	42.28	46-19	49.48	53 49	56.33	62.49	65.00
34	33-34	35.44	37.80	40.68	44.90	48·60	51.97	56.06	58-96	65.25	6 <del>7</del> -80
36	35.34	37.50	39.92	42.88	47:21	51.00	54.44	58.62	6x·58	67.99	70.59
38	37:34	39.56	42.05	45.08	49.21	23.38	56·90	61.16	64 18	70-70	73:35
40	39-34	41.62	44-16	47:27	51.81	55.76	WO. 0.	60.60	CC		
50	49:33	51.89	54.72	58.16	63.12		59.34	63.69	66.77	73.40	76.09
60	59·33	62.13	54 74 65:23	68.97	74.40	67·50	71.42	76·15	79.49	86.66	89.56
70	69.33	72.36	75.69	79.71	85.23	79.08	83.30	88.38	91.95	99.61	102.7
80	79:33	82.57	86-12	90.41	96.28	90.23	95.02	100.4	104.2	112.3	115.6
-	17 33	J# 3/ .	30 12	90.41	90-50	101.0	106.6	112.3	116.3	124.8	128.3
90	89.33	92.76	96-52	101.1	107.6	113.1	118·1	124.1	128.3	137.2	140.8
100	99.33	102.0	106.9	111.2	118-5	124.3	129.6	135.8	140.2	149.4	153.5

Denominator									N	umerate	or	
df	2	3	4	5	6	7	8	9	10	11	12	13
1	8.93	13.44	16.36	18.49	20.15	21.50	22.64	23.62	24.48	25.24	25.92	26.5
2	4.13	5.73	6.77	7.54	8.14	8.63	9.05	9.41	9.73	10.01	10.26	10.4
3	3.33	4.47	5.20	5.74	6.16	6.51	6.81	7.06	7.29	7.49	7.67	7.83
. 4	3.02	3.98	4.59	5.04	5.39	5.68	5.93	6.14	6.33	6.49	6.65	6.78
5	2.85	3:72	4.26	4.66	4.98	5.24	5.46	5.65	5.82	5.97	6.10	6.2
6	2.75	3.56	4.07	4.44	4.73	4.97	5.17	5.34	5.50	5.64	5.76	5.8
7	2.68	3.45	3.93	4.28	4.56	4.78	4.97	5.14	5.28	5.41	5.53	5.6
8	2.63	3.37	3.83	4.17	4.43	4.65	4.83	4.99	5.13	5.25	5.36	5.40
9	2.59	3.32	3.76	4.08	4.34	4.55	4.72	4.87	5.01	5.13	5.23	5.3
10	2.56	3.27	3.70	4.02	4.26	4.47	4.64	4.78	4.91	5.03	5.13	5.2
11	2.54	3.23	3.66	3.97	4.21	4.40	4.57	4.71	4.84	4.95	5.05	5.1
12	2.52	3.20	3.62	3.92	4.16	4.35	4.51	4.65	4.78	4.89	4.99	5.08
13	2.50	3.18	3.59	3.89	4.12	4.30	4.46	4.60	4.72	4.83	4.93	5.02
14	2.49	3.16	3.56	3.85	4.08	4.27	4.42	4.56	4.68	4.79	4.88	4.9
15	2.48	3.14	3.54	3.83	4.05	4.24	4.39	4.52	4.64	4.75	4.84	4.9
16	2.47	3.12	3.52	3.80	4.03	4.21	4.36	4.49	4.61	4.71	4.81	4.8
17	2.46	3.11	3.50	3.78	4.00	4.18	4.33	4.46	4.58	4.68	4.77	4.8
18	2.45	3.10	3.49	3.77	3.98	4.16	4.31	4.44	4.55	4.65	4.75	4.8
19	2.45	3.09	3.47	3.75	3.97	4.14	4.29	4.42	4.53	4.63	4.72	4.8
20	2.44	3.08	3.46	3.74	3.95	4.12	4.27	4.40	4.51	4.61	4.70	4.7
21	2.43	3.07	3.45	3.72	3	4.11	4.26	4.38	4.49	4.59	4.68	4.7
22	2.43	3.06	3.44	3.71	3.92	4.10	4.24	4.36	4.47	4.57	4.66	4.7
23	2.42	3.05	3.43	3.70	3.91	4.08	4.23	4.35	4.46	4.56	4.64	4.7
24	2.42	3.05	3.42	3.69	3.90	4.07	4.21	4.34	4.45	4.54	4.63	4.7
25	2.42	3.04	3.42	3.68	3.89	4.06	4.20	4.32	4.43	4.53	4.61	4.6
26	2.41	3.04	3.41	3.68	3.88	4.05	4.19	4.31	4.42	4.52	4.60	4.6
27	2.41	3.03	3.40	3.67	3.87	4.04	4.18	4.30	4.41	4.50	4.59	4.6
28	2.41	3.03	3.40	3.66	3.87	4.03	4.17	4.29	4.40	4.49	4.58	4.6
29	2.40	3.02	3.39	3.65	3.86	4.02	4.16	4.28	4.39	4.48	4.57	4.6
30	2.40	3.02	3.39	3.65	3.85	4.02	4.16	4.28	4.38	4.47	4.56	4.64
40	2.38	2.99	3.35	3.61	3.80	3.96	4.10	4.22	4.32	4.41	4.49	4.5
60	2.36	2.96	3.31	3.56	3.76	3.91	4.04	4.16	4.25	4.34	4.42	4.49
80	2.35	2.95	3.29	3.54	3.73	3.89	4.01	4.13	4.22	4.31	4.39	4.4
120	2.34	2.93	3.28	3.52	3.71	3.86	3.99	4.10	4.19	4.28	4.35	4.4
240	2.34	2.92	3.26	3.50	3.68	3.83	3.96	4.07	4.16	4.24	4.32	4.3
∞ ′	2.33	2.90	3.24	3.48	3.66	3.81	3.93	4.04	4.13	4.21	4.29	4.35

NMI